In-bore setup and software for 3T MRI-guided transperineal prostate biopsy

Junichi Tokuda\textsuperscript{1}, Kemal Tuncali\textsuperscript{1}, Iulian Iordachita\textsuperscript{2}, Sang-Eun Song\textsuperscript{1}, Andriy Fedorov\textsuperscript{1}, Sota Oguro\textsuperscript{1}, Andras Lasso\textsuperscript{3}, Fiona M Fennessy\textsuperscript{1}, Clare M Tempany\textsuperscript{1} and Nobuhiko Hata\textsuperscript{1}

\textsuperscript{1} Department of Radiology, Brigham and Women’s Hospital and Harvard Medical School, Boston, MA, USA
\textsuperscript{2} Laboratory for Computational Sensing and Robotics, Johns Hopkins University, Baltimore, MD, USA
\textsuperscript{3} School of Computing, Queen’s University, Kingston, ON, Canada

E-mail: tokuda@bwh.harvard.edu

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Abstract

MRI-guided prostate biopsy in conventional closed-bore scanners requires transferring the patient outside the bore during needle insertion due to the constrained in-bore space, causing a safety hazard and limiting image feedback. To address this issue, we present our custom-made in-bore setup and software to support MRI-guided transperineal prostate biopsy in a wide-bore 3 T MRI scanner. The setup consists of a specially designed tabletop and a needle-guiding template with a Z-frame that gives a physician access to the perineum of the patient at the imaging position and allows the physician to perform MRI-guided transperineal biopsy without moving the patient out of the scanner. The software and Z-frame allow registration of the template, target planning and biopsy guidance. Initially, we performed phantom experiments to assess the accuracy of template registration and needle placement in a controlled environment. Subsequently, we embarked on our clinical trial ($N = 10$). The phantom experiments showed that the translational errors of the template registration along the right–left (RP) and anterior–posterior (AP) axes were $1.1 \pm 0.8$ and $1.4 \pm 1.1$ mm, respectively, while the rotational errors around the RL, AP and superior–inferior axes were $(0.8 \pm 1.0)^\circ$, $(1.7 \pm 1.6)^\circ$ and $(0.0 \pm 0.0)^\circ$, respectively. The 2D root-mean-square (RMS) needle-placement error was 3 mm. The clinical biopsy procedures were safely carried out in all ten clinical cases with a needle-placement error of 5.4 mm (2D RMS). In conclusion, transperineal prostate biopsy in a wide-bore 3T scanner is feasible using our custom-made tabletop setup and software, which supports manual needle placement without moving the patient out of the magnet.

(Some figures may appear in colour only in the online journal)
1. Introduction


The type of needle-placement approach, either transrectal or transperineal, is an important factor that affects applicability to patients, accessibility to targets in the prostate gland and invasiveness in MRI-guided prostate biopsy. While devices to support transrectal approach has commercially been available and have been used in several clinical studies (Beyersdorff et al 2002, Engelhard et al 2006), the transperineal approach has also been investigated because of its better access to anterior and apical regions (Sartor et al 2008) and its applicability to patients, who cannot undergo TRUS-guided biopsy due to previous total colectomy. MRI-guided transperineal biopsy was first reported by D’Amico et al using an open-configuration 0.5 T MRI scanner (D’Amico et al 2000, Cormack et al 2000, Hata et al 2001). The open-configuration MRI magnet was ideal for transperineal approach, since it allowed the radiologist direct access to the patient’s perineum in lithotomy position in the magnet throughout the procedure. As the subject stayed in the scanner, real-time MRI allowed monitoring the needle continuously during the needle-insertion process, significantly improving the accuracy of the needle placement and hence targeting.

The successful demonstration of MRI-guided transperineal prostate biopsy in this unique 0.5 T MRI scanner led other groups to investigate the use of conventional closed-bore scanners also for transperineal biopsy to take advantage of better image quality and wider availability of those scanners (Susil et al 2004, Menard et al 2011, 2010). However, conventional closed-bore scanners require to transfer the subject outside the bore during transperineal needle insertion, as there is limited access to the perineum due to the constrained in-bore space. Thus, there is no visual feedback during needle insertion, which is further complicated by the repeated patient transfer during a procedure. Recent advancements in magnet technologies have allowed
scanner manufacturers to design high-field closed-bore magnets with wider (70 cm) and shorter gantries that provide better access to the patient’s perineum with superior image quality. To the best of our knowledge, there has been no custom-designed in-bore setup or navigation software to facilitate MRI-guided manual prostate biopsy using the transperineal approach, except for computer-controlled robotic devices (Fischer et al 2008, Song et al 2012, van den Bosch et al 2010, Muntener et al 2008, Cunha et al 2010), which still require further investigations to be used safely and regularly without any help from robotic specialists.

Thus, we developed such an in-bore setup and software that enables transperineal prostate biopsy in a wide and closed-bore 3T MRI scanner with the patient in the lithotomy position. Our goal was to attain better control of the needle insertion and minimize the safety hazard or special perioperative arrangement to bring the patient in and out of scanner bore. We also developed planning and navigation software to obtain MRI from the scanner by online connection and perform target planning, template registration and monitoring of the needle placement. We tested the overall template registration and needle-placement accuracy in a pre-clinical phantom validation study, and subsequently applied our methodology to ten clinical cases.

2. Materials and methods

2.1. Prostate intervention table with needle-guiding template

We designed and built a prostate intervention tabletop setup with built-in leg supports to allow the subject to be positioned in the lithotomy position in the scanner (figure 1). The tabletop was specifically designed to fit in a wide-bore (70 cm diameter) MRI scanner (MAGNETOM Verio 3T, Siemens AG, Erlangen, Germany). The patient is placed in the feet-first position to keep the patients face on the front side of the scanner, allowing the anesthesiologist and the vital monitor device to stay on the same side throughout the procedure. With this arrangement, the radiologist stands at the bore entrance on the back side of the scanner to reach the perineum of the patient. The tabletop consists of base board, leg supports, a needle-guiding template and a Z-shaped calibration marker (Z-frame) (DiMaio et al 2007). The baseboard is a wooden or plastic plate designed to fit on the patient table of the MRI scanner. The leg holders, attached to the baseboard by adjustable attachment, keep the legs apart and raised. The height of the tabletop from the floor of the scanner room is 91 cm, while the distance between the edge of the tabletop and the perineum was 76 cm. This configuration allows the radiologist to easily reach the perineum from the edge of the tabletop at the entrance of the bore of the MRI scanner (figure 1).

The needle-guiding template, originally developed for prostate cancer brachytherapy, is an acrylic block with dimensions of 100 × 120 × 25 mm³ with a grid of 1.3 mm diameter holes spaced 5 mm apart. It is fixed in the middle of the prostate intervention table located between the patient’s legs and secured close to the subjects perineum. The template is supported by a two-degree-of-freedom (2-DOF) adjustable holder, which allows movement of the template in craniocaudal and anteroposterior directions. The Z-frame is attached in a predefined position to the template and is detached after calibration.

2.2. Calibration of needle-guiding template by Z-frame registration

The template is calibrated to the MRI coordinate system by imaging the Z-frame affixed to the template. The Z-frame has seven rigid tubes with 7.5 mm inner diameters filled with a contrast agent (MR Spots, Beekley, Bristol, CT) placed on three adjacent faces of a 60 mm cube, thus forming a Z-shaped enhancement in the images. It is registered by digitizing the
Figure 1. The photographs show (A) the overview of the prostate intervention table with leg supports during the clinical case, (B) the leg support, base board and stationary frame installed on the patient table of the scanner, (C, D) the front and rear view of the template with the Z-shaped calibration frame (Z-frame), (E) the close-up of the Z-frame and (F) the scene, where the radiologist was reaching the perineum during the procedure. The template is supported by a 2-DOF adjustable holder, which allows shifting the template in the cranio-caudal (CC) and anteroposterior (AP) directions indicated by the arrows in (C).

The hyper-intensity cross-section of the tubes in the marker to register the Z-frame to the MRI coordinate system. The seven rigid tubes are automatically detected on cross-sectional MRI images of the Z-frame, providing the location and orientation of the Z-frame in the MRI coordinate system (figure 2). We used the 3D fast low angle shot (FLASH) imaging sequence for calibration (TR/TE: 12 ms/1.97 ms; acquisition matrix: 256 × 256; flip angle 45°; field of view: 160 × 160 mm²; slice thickness: 2 mm; receiver bandwidth: 400 Hz/pixel; number of averages: 3). The positions and orientations of the Z-frame calculated from the image slices that show the section of the seven rigid tubes were averaged. Once the Z-frame is registered to the MRI coordinate system, the geometric correlation between the template and the patient anatomy becomes known, enabling the selection of a hole that will guide a biopsy needle to a target previously defined by multi-parametric MR imaging. After the template is calibrated, the Z-frame is detached.
2.3. Navigation software

We developed planning and navigation software for MRI-guided prostate biopsy as a plug-in software module for the open source medical image-processing and visualization software 3D slicer (http://www.slicer.org) (Gering et al 2001) to provide an integrated console to perform the following processes: (1) target planning based on preprocedural images, (2) image registration of preprocedural images and intraprocedural images, (3) needle-placement planning, (4) registration of the template using MR images of the Z-frame, (5) hole position calculation and (6) confirmation of needle placement. For image registration, we used B-spline non-rigid registration (Rueckert et al 1999) with maximization of mutual information (Mattes et al 2003) available as part of the BRAINSFit plug-in module (Johnson et al 2007) in 3D slicer. The image registration in process (2) also includes registration of planned targets defined on a preprocedural image prior to a procedure; the software applies a transformation that registers the preprocedural image to the intraprocedural image to map the target onto the intraprocedural image. In process (5), the hole positions and needle insertion depth for needle placement are calculated based on the target mapped onto the intraprocedural image, and the position and orientation of the template in the image coordinate system given by the template registration in process (4). For confirmation of needle placement in process (6), MR images of the placed needle is acquired and imported to the navigation software, where it is overlaid onto the intraprocedural image. The radiologist visually confirms the needle position and determines if reposition of the needle is necessary.

2.4. Preclinical validation studies

We conducted two phantom experiments in the wide-bore 3T MRI scanner to assess (1) the accuracy of Z-frame registration and (2) the overall accuracy of needle placement using a phantom. These studies investigated the feasibility of accurate needle placement using the template and Z-frame in a controlled environment.
Accuracy of Z-frame registration. We evaluated the translational registration error $\Delta t$ and rotational registration error around the center of the Z-frame $\Delta \theta$ of the Z-frame registration. We also estimated the target registration error (TRE) to predict the largest possible targeting error of biopsy needle placement. The translational and rotational registration errors are defined as

$$\Delta t = t_I - t_P,$$

$$\Delta \theta = \arccos(R_Pn \cdot R_In),$$

where $R_P$ and $t_P$ are the physical rotation matrix and the physical translation vector of the Z-frame (gold standard), $R_I$ and $t_I$ are the rotation matrix and the translation vector of the Z-frame detected by the Z-frame registration method described above, $n$ is a normal vector perpendicular to the axis of rotation $R_P$. The TRE is defined as the error between the needle tip position expected from the physical rotation and translation of the Z-frame and the needle tip position estimated from the rotation and translation of the Z-frame detected by the Z-frame registration method defined as

$$\text{TRE} = (R_Iv + t_I) - (R_Pv + t_P),$$

where $v$ is the translation vector representing the relative position of the needle tip with respect to the Z-frame coordinate system. In this study, $R_P$ and $t_P$ indicate the physical location of the Z-frame on the acrylic base with respect to the MR scanner. The acrylic base was first calibrated with the isocenter of the imaging bore using land-marking laser available in the scanner. The values of $R_P$ and $t_P$ were then found by aligning the Z-frame to the graduations printed on the acrylic base. The graduations allows the Z-frame to be placed at 0, 50, 100, 150 and 200 mm horizontally off the isocenter of the imaging bore, and tilted 0$^\circ$, 5$^\circ$, 10$^\circ$, 15$^\circ$ and 20$^\circ$ horizontally from the main magnetic field. To evaluate the accuracy of Z-frame registration, while shifting the Z-frame along the Z-frames $x$- and $y$-axes and rotating around the Z-frames $x$-, $y$- and $z$-axes (roll, pitch and yaw, respectively), we placed the Z-frame on the acrylic base with respect to the MRI coordinate system as illustrated in figure 3. The shift along the $z$-axis, which corresponds to the SI axis in the MRI coordinate system, was not considered in this experiment, since the MRI scanner automatically positions the imaging subject to its isocenter by moving the table. Prior to shifting or rotating the Z-frame, the base with the graduation was calibrated in the MRI coordinate system by performing the Z-frame registration with placing the Z-frame at 0 mm off the center and 0$^\circ$ tilt from the main magnetic field. The amount of shifts along $x$- and $y$-axes and the roll, pitch and yaw rotations were varied independently to calculate $\Delta t$ and $\Delta \theta$ using equation (1) and (2). For each shift and rotation, eight sets of 3D images of the Z-frame were acquired and processed to estimate the position and orientation of the Z-frame. The frequency and phase encoding directions were aligned to the $x$- and $y$-axes of the Z-frame, respectively, at the initial position (position and orientation before applying any shift or rotation) in order to simulate the image orientation in the clinical application, where the orientation of the Z-frame image is set to axial with respect to the patient (or MRI) coordinate system. A total of 240 images were acquired. In addition, the TRE was estimated assuming that the distance between the target and the center of the Z-frame was a needle length of 100 mm. In all measurements, average and standard deviation were computed and tabulated.

Accuracy of needle placement in the mock procedure. In our second experiment, we performed a second procedure using a prostate phantom (Model 053 Ultrasound Prostate Training Phantom, Computerized Imaging Reference Systems, Inc., Norfolk, VA) that mimics a gland, urethra, seminal vesicles and rectum on an MR image. The objective of this experiment
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Figure 3. (A) The relationship between the Z-frame coordinate system (x, y, z) and the image coordinate system (R, A, S) in the clinical application is illustrated. The image coordinate system is defined, where the patient is positioned in feet-first, supine position in the magnet. To evaluate the accuracy of Z-frame registration, while shifting the Z-frame along the Z-frames x- and y-axes and rotated around the Z-frames x- and y-axes (roll, pitch and yaw, respectively), the Z-frame on the acrylic base in three ways as illustrated above; the x-, y- and z-axes of the Z-frame were initially aligned to: (B) the RL-, AP- and SI-axes of the image coordinate system, respectively, to shift the Z-frame along the x-axis as well as rotate around the y-axis (pitch) of the Z-frame; (C) the AP-, RL- and SI-axes, respectively, to shift along the y-axis as well as to rotate around the x-axis (roll); (D) the RL-, SI- and AP-axes, respectively, to rotate around the z-axis (yaw).

was to evaluate the overall accuracy of needle placement in mock biopsy procedures in a controlled environment. The prostate phantom was placed in the magnet in a typical location of the prostate during a clinical procedure. The template with the Z-frame was fixed in front of the phantom so that the distance between the surface of the phantom and virtual targets defined in the phantom ranged from 60 to 120 mm. In each procedure, the image of the phantom and the Z-frame was acquired using a 3D FLASH sequence as described in the previous section, followed by the image of the phantom with a 2D turbo spin echo (TSE) sequence (TR/TE = 5250/100 ms; acquisition matrix = 320 × 224; flip angle = 150°; field of view = 160 × 160 mm²; slice thickness = 3 mm; receiver bandwidth = 205 Hz/pixel). Those images were then loaded into 3D slicer to register the template to the MRI coordinate system and to define virtual targets in the prostate phantom. The virtual targets were randomly picked within each of eight segments in the mock prostate in the phantom, as indicated in figure 4. A total of eight virtual targets were defined for each procedure. 3D slicer determined the needle hole position and the insertion depth from the target positions. After a 18-gauge × 15 cm high-nickel-content stainless steel needle with diamond-shaped tip (MRI Bio Gun, E-Z-EM, Westbury, NY) was inserted, a confirmation image was acquired around the target with a half-Fourier acquisition single shot turbo spin echo (HASTE) sequence (TR/TE = 1000 ms/102 ms; matrix = 320 × 179; flip angle = 150°; field of view = 280 × 224 mm²; slice thickness = 2 mm; receiver bandwidth = 780 Hz/pixel; acquisition time: 1 s) along the axial and the sagittal plane in order to measure the distance between the defined target and the center...
Figure 4. Eight targets were defined on the periphery of the mock prostate in the phantom. Each target was randomly picked up within each of segments A–H as indicated above. The diameter of the mock prostate was approximately 40 mm.

of the needle artifact on the same axial plane and to obtain 2D needle-placement error. The single shot turbo spine echo sequence was selected for this evaluation because our previous study demonstrated that the axis of the needle could accurately be localized by the artifact with an error of less than the level of pixel size (1 mm) when the needle was placed in parallel to the static field (DiMaio et al. 2006). Four mock procedures were performed, resulting in a total of 32 biopsies in the study. Two types of error were evaluated retrospectively: targeting error, defined by the distance between the planned target position and the center of the needle artifact on the needle confirmation image; needle-placement error, defined by the distance between the ‘expected needle position’ and the center of the needle artifact. The expected needle position was the needle position reachable from the needle hole and needle insertion depth determined by 3D slicer. Therefore, the difference between the targeting error and the needle-placement error is whether they take into account the effect of the 5 mm gap between the holes on the template. 2D root mean square (RMS) of both targeting error and needle-placement error was computed for each segment in figure 4, as well as for all 32 biopsies.

2.5. Clinical studies

We conducted an investigation during initial clinical studies to assess the safety and feasibility of the methods developed. Ten men (age range: 50–73 years; weight range: 147–211 lbs) underwent targeted core biopsy of the prostate in the wide-bore 3T MRI scanner. The study protocol was approved by the Brigham and Womens Hospitals Institutional Review Board prior to patient enrollment and was HIPAA compliant. The patients with suspicious foci were eligible for the study after undergoing a multi-parametric 3T MRI examination with endorectal coil. All patients had elevated serum prostate specific antigen (PSA) and a dominant index lesion (most suspicious for cancer) on recent diagnostic 3T prostate MRI. Index lesions were depicted as a focus of decreased T2 signal on T2-weighted imaging (T2WI), restricted diffusion on diffusion weighted imaging (DWI), and early arterial phase enhancement with rapid wash-out on dynamic contrast enhanced (DCE) sequences. Clinical indications included: inability to obtain TRUS-guided biopsy due to total colectomy (N = 1) or inflamed ileal J-pouch (N = 1), multiple prior negative TRUS-guided biopsies (N = 6), prior prostate brachytherapy and MRI focus suspicious for recurrence (N = 1), and MRI focus suspicious for higher
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Figure 5. The system configuration and the data flow before and during the procedure is shown. For preprocedural planning, which took place a few days before the procedure, preprocedural MRI data, including T2W, DCE, and diffusion-weighted images were retrieved from the hospital’s picture archiving and communication system (PACS). The radiologists identified the suspicious foci as biopsy targets based on the preprocedural MRI. During the procedure, intraprocedural T2W MRI acquired by the MRI scanner in the operating room was transferred from the host workstation to the navigation workstation for intraprocedural planning and the image-processing workstation for registering the preprocedural MRI and the biopsy targets to the intraprocedural MRI. The registered preprocedural MRI and registered targets were returned to the navigation workstation for the radiologists review and calculation of the template hole index and depth for guiding the needle.

grade tumor than suggested at prior TRUS-guided biopsy (N = 1). Informed consent for the procedure was obtained from each subject after the nature of the procedure and the potential hazards had been fully explained. The system configuration and flow of data before and during the procedure are shown in figure 5. The workflow of the procedure was as follows.

- **Preprocedural planning.** Two radiologists reviewed preprocedural multi-parametric MRI exams, consisting of T2-weighted MRI, pharmacokinetic parameter maps obtained from DCE-MRI, and apparent diffusion coefficient (ADC) maps calculated from diffusion-weighted MRI, to identify suspicious targets. These preprocedural images and the preprocedural targets were stored in the image-processing workstation for intraprocedural image registration.

- **Patient preparation.** On the day of the biopsy, the patient was taken to the 3T MRI with a 70 cm wide-bore (MAGNETOM Verio 3T, Siemens AG, Erlangen, Germany) and placed supine on the prostate intervention table in feet-first orientation so that the radiologist could approach the perineum from the other side of the magnet. The leg supports were adjusted and fixed, the patient was positioned in the lithotomy position, and the imaging
coil (Body Matrix Coil, Siemens AG, Erlangen, Germany) was placed over the anterior lower pelvis on the front side of the scanner. The patient was then transferred to the other side of the magnet in the far end of the room, where the perineum was prepped and draped in a sterile fashion. The sterile stationary frame and the template with the Z-frame were set up. When the radiologist confirmed that all instruments were properly adjusted, the patient was moved into the isocenter of the magnet for imaging. The procedures were performed under standard departmental guidelines using intravenous conscious sedation (typically using Versed and Fentanyl).

- **Pre-procedural MRI and planning in 3D slicer.** Two sets of MR images were acquired after the patient was positioned in the isocenter of the magnet. The first was a 3D image of the Z-frame acquired by a 3D FLASH sequence with the same parameters used in the preclinical study. The Z-frame image was transferred to the navigation workstation for localization of the Z-frame as described above. The second image was an intraprocedural 2D multi-slice T2-weighted (T2W) image of the prostate acquired by TSE sequence with the same parameters as the preclinical study. The intraprocedural T2W image was acquired while the Z-frame was being localized on the navigation workstation. The intraprocedural T2W prostate image was transferred to the navigation workstation, where the radiologist identified suspicious foci shown in the T2 image as intraprocedural targets. While the radiologist was reviewing the intraprocedural T2W prostate image, the image was also transferred to the image-processing workstation in order to register the preprocedural T2W image to the intraprocedural T2 image using the B-spline deformable image registration (Oguro et al 2009, Fedorov et al 2012). Including manual cropping of the region of interest, it took 5–10 min to register the preprocedural T2W image to the intraprocedural T2W image. The detail of the deformable image registration methodology is described in our separate report (Fedorov et al 2012). The planning and registration processes were performed in parallel to minimize time. The transformation derived from the deformable image registration was then used to register the preprocedural targets to the intraprocedural T2W MRI. Once all the intraprocedural targets and preprocedural targets were projected on the intraprocedural T2W image, 3D slicer selected the optimal template holes for inserting the biopsy needle and the insertion depth of the needles.

- **Needle placement and monitoring.** After the Z-frame was detached from the template, the radiologist first applied local anesthetic and then inserted an 18-gauge × 15 cm MRI-compatible core biopsy needle (one of the following three types: MRI Bio Gun, E-Z-EM, Westbury, NY; Single Action Biopsy Device, US Biopsy, Franklin, IN; Semi Automatic Biopsy Gun, Invivo, Schwerin, Germany; Fully Automatic Biopsy Gun, Invivo, Schwerin, Germany) through the selected hole until it reached the calculated insertion depth. The depth of the needle insertion was previously marked on the outer shaft of the needles by the radiologist. Once the needle was inserted, a 2D needle confirmation image was obtained in either the axial or the coronal plane at the planned target position using either 2D Turbo FLASH sequence (TR/TE = 402.21 ms/1.45 ms; acquisition matrix = 128 × 115; flip angle = 140°; field of view = 200 × 200 mm²; slice thickness = 3 mm; receiver bandwidth = 1500 Hz/pixel; imaging time: 400 ms) (cases 1–8) or 2D multislice TSE (TR/TE = 2700 ms/106 ms; acquisition matrix = 280 × 280; flip angle = 48°; field of view = 200 × 200 mm²; slice thickness = 3 mm; receiver bandwidth = 252 Hz/pixel; imaging time: approx. 1 min) (cases 9, 10) to confirm that the needle was placed at the desired position. If the needle was not found to be close enough to the target lesion, the needle was reinserted through an alternative hole selected based on MR image guidance. Upon satisfactory placement of the needle tip over the target based upon MR, the tissue samples were collected, labeled and sent for site-specific pathological examination.
Figure 6. The translational and rotational registration errors in Z-frame registration, when the Z-frame was placed at 0, 50, 100, 150, and 200 mm horizontally off the isocenter along the x- and y-axes of the Z-frame, and tilted 0°, 5°, 10°, 15° and 20° in roll, pitch and yaw of the Z-frame (N = 8).

- **Evaluation of needle placement accuracy.** The targeting error and the needle placement error (see the section *Accuracy of needle placement in the mock procedure* for definitions) were retrospectively measured to investigate the needle-placement precision, which can vary due to the 5 mm gap between needle insertion holes. Since the core biopsy needle cuts a 20 mm length of tissue along the needle axis, the accuracy of needle placement was evaluated within the axial plane, which is approximately perpendicular to the needle. The average and standard deviation of placement accuracy were computed as RMS from all needle insertion trials and were tabulated. In addition, as secondary measurements, numbers of target sites and time taken per procedure were recorded and averages were tabulated.

3. Results

3.1. Preclinical validation studies

The translational registration error along the x- and y-axes and the rotational registration error in roll, pitch and yaw are shown in figure 6; the overall translational errors were $-1.1 \pm 0.8$ mm for the x-direction and $-1.4 \pm 1.1$ mm for the y-direction corresponding to RL and AP directions of the patient, respectively (see figure 6). The rotational errors were $(0.8 \pm 1.0)^\circ$ in roll, $(−1.7 \pm 1.6)^\circ$ in pitch and $(0.0 \pm 0.0)^\circ$ in yaw, corresponding to the rotations around RL-, AP- and SI-axes in the clinical setting. The expected TRE for a 100 mm needle are shown in figure 7. In the mock procedure, the RMS targeting error was 3.0 mm, while the RMS needle-placement error was 2.4 mm. The relationship between the targeting error and the location of the target in the prostate in the mock procedure is shown in figure 8.

3.2. Clinical study

All ten procedures were technically successful and patients tolerated the procedure well without intraprocedural or postprocedural pain. Table 1 summarizes the needle-placement accuracy per case. Two patients had asymptomatic self-limited small periprostatic hematoma on imaging. No other complications were encountered. For each patient, two–five targets were
Figure 7. The 2D expected TRE of Z-frame registration for a 100 mm needle are shown. For the left graph, the Z-frame was placed at 0, 50, 100, 150 and 200 mm off center in the x- and y-directions ($N = 4$ for each distance), while the orientation of the Z-frame was fixed to the original direction (no tilt in any direction). For the right graph, the Z-frame was tilted $0^\circ$, $5^\circ$, $10^\circ$, $15^\circ$ and $20^\circ$ in roll, pitch and yaw of the Z-frame ($N = 8$), while the center of the Z-frame was fixed at the isocenter. In this evaluation, all translational and rotational errors were taken into account.

Table 1. The results of needle placement in the ten clinical cases including the number of targets, the targeting error, the needle-placement error are shown. All errors were measured in the 2D axial plane at the planned target and shown as RMS errors. The 2D RMS targeting error and needle-placement error through the ten cases were 5.4, and 5.7 mm respectively.

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identified on pre-biopsy MR images and selected for biopsy. MR images from a clinical case are shown in figure 9. Despite the lack of an endorectal coil, the images provide sufficient contrast of the prostate and its substructures, allowing us to perform automatic deformable registration of the preprocedural and intraprocedural MRI with acceptable accuracy, reliability and computation time (Fedorov et al 2012). The quality of tissue core samples was acceptable by visual observation during the procedure. Tissues were sampled from an average of four locations in 104 min per procedure. The 2D RMS targeting error was 5.4 mm, while the RMS needle-placement error was 5.7 mm. The duration of the procedures ranged from 65 to 130 min including 25–70 min of preparation, e.g., patient setup and coil placement. In some studies, such as case 5, movement of the patients led to repositioning of the template and the coil, prolonging the time for setup.
4. Discussion

We have developed and report here a prostate intervention apparatus and compatible software to support transperineal manual needle placement into the prostate in a wide-bore 3T MRI scanner. The in-bore tabletop setup and software can also be used for prostate therapy techniques, such as brachytherapy, laser ablation, or cryoablation, since these therapies are performed using the transperineal approach rather than transrectal. We performed both a phantom study to investigate the accuracy of needle placement and a preliminary clinical study to assess the accuracy, safety and feasibility of the procedure, the equipment and software. The contributions of this paper are the novel engineering solutions that allow us to perform accurate core needle prostate biopsy, and accuracy assessment of template registration and needle placement in both phantom and patients. To the best of our knowledge, only a limited number of previous studies have assessed the needle-placement accuracy for MRI-guided transperineal template biopsy and interventions in patients (Susil et al 2004, Blumenfeld et al 2007, Menard et al 2010), animal (Lakosi et al 2009) and cadavers (Woodrum et al 2010), and none of them have performed comprehensive accuracy evaluation including...
calibration of guidance tools and needle placement in phantoms and patients, except the work of Blumenfeld et al (2007). It would also be desirable to further investigate other source of errors, e.g., geometric accuracy of the MRI scanner, tissue deformation and needle deflection for this particular application.

One of the important benefits of intraprocedural 3T MRI is its superior image quality, which is ideal for accurate fusion of preprocedural diagnostic MRI and intraprocedural guidance image. Mapping preprocedural MRI onto the guidance image has been of major clinical interest; several groups have demonstrated image fusion of preprocedural diagnostic MRI with intraprocedural TRUS (Ukimura et al 2010, Natarajan et al 2011) or intraprocedural MRI (Hambrock et al 2008, Franiel et al 2011). While these investigators have used rigid registration (Ukimura et al 2010), surface shape (Natarajan et al 2011) or visual assessment (Hambrock et al 2008, Franiel et al 2011), our study demonstrated that automatic deformable registration is indeed feasible for pre- and intraprocedural MRI fusion. We have reported the detail of our intraprocedural automated deformable image registration methodology with an average in-slice landmark registration error of 1.3 ± 0.5 mm and computation time of at most 2 min (Fedorov et al 2012). Mapping preprocedural MRI onto guidance images is desirable even for a procedure guided by such state-of-the-art 3T MRI, because often it is not practical to perform multiparametric MRI study and MRI-guided biopsy in the same imaging session due to time constraints. This outcome leads us to believe that our method allows for a precise site-specific pathological correlation with MR image abnormalities. This feature is critical for providing tissue validation of the pre-biopsy MR image parameters; this would only be available otherwise through radical prostatectomy, with image registered to whole-mount pathology of the gland specimen. This analysis is not easily obtained and certainly not available in all men as they do not all undergo surgery.

The accuracy study on Z-frame registration showed that the translational error of the Z-frame registration was 1.4 mm along the axis plane, and 0.8° maximum in axial plane rotation, which are comparable to other studies using fiducials for calibration (Dumoulin et al 1993, Engelhard et al 2006, Patil et al 2009, Rea et al 2008). There are several factors that may affect the accuracy of the Z-frame registration. First, a degraded signal-to-noise ratio due to the selection of the coil may affect the accuracy of Z-frame registration; our previous study of Z-frame registration using a head coil (DiMaio et al 2007) showed better registration accuracy than this study probably due to the better signal-to-noise ratio of the head coil. In this study, the body matrix coils were used in a 3T scanner to cover both the pelvic area and the Z-frame in the clinical setting. It is of our interest to assess the impact of image quality on the accuracy of registration in the future. Second, the geometric accuracy of images from the wide- and short-bore MRI scanner due to the field inhomogeneity is another possible source of the Z-frame registration error. Although further investigation is required to quantify it, our result (figure 6) suggests that it is not a major concern in our clinical application, because the translational error of the Z-frame registration did not change dramatically within 15 cm from the isocenter, which covers the typical positions of the Z-frame and the area of the prostate gland. Third, the rotational error also depends on the orientation of the rotation; the error in the rotation around the SI-axis was significantly smaller than the errors for the other axes. This can be explained by the fact that the rotation around the SI-axis is in-plane with respect to the slice of the Z-frame images, while the others are out-of-plane. If $\theta$ and $d$ are the rotational angle and the size of the Z-frame cube, respectively, the in-plane rotation is associated with the shift of the bright spots proportional to $\theta d/2$ on the Z-frame image, while the out-of-plane rotations are associated with the change of the distances between the bright spots proportional to $d(1 - \cos(\theta))/2$. Consequently, in-plane motion causes larger shift of the bright spots on the image when $\theta$ is sufficiently small. Adding diagonal tubes on the superior and inferior
faces of the cube and acquiring images in the three orthogonal planes would help improve the rotational accuracy of the Z-frame registration. Fourth, the limited length of the tubes filled with the contrast agent attached to the Z-frame limits the range of tilting angle that is accurately detected by the Z-frame registration. Because we chose to use the commercially available approved makers to build our Z-frame with the scope of the clinical application, the tube was not sufficiently long for the diagonal rod of the Z-frame; it was difficult to maintain all three diagonal tubes within the axial imaging plane, especially when the Z-frame was rotated around the y-axis (or in pitch) by a large angle. This may explain why we observed a larger error in rotations in pitch than that in roll and yaw.

In our mock procedures, we found that the RMS targeting error was 3.0 mm, while the RMS needle-placement error was 2.4 mm. This indicates that the inaccuracy of needle targeting was caused primarily by Z-frame registration and needle deflection (2.4 mm), while the error due to the limited number of needle insertion holes is less. The RMS error expected from the Z-frame registration error was within 2.5 mm, while the Z-frame was less than 100 mm from the isocenter (figure 7); this result suggests that the needle deflection contributed to the targeting error. This result is comparable to our previous study (Blumenfeld et al 2007), where the template registration error was responsible for 1.5 ± 0.3 mm of needle-placement error and needle deflection was responsible for 0.6 — 1.1 mm of placement error.

Our clinical study shows that the technique is feasible in its ability to approach the prostate gland transperineally in a 3T scanner, utilizing the lithotomy position while keeping the patient inside the magnet for repeated imaging. It allows needle placement with 5.4 mm accuracy in clinical biopsies, which was superior to our previous clinical study using 18-gauge needle in the 0.5 T MRI scanner, where the targeted biopsy error was 6.5 ± 3.5 (Blumenfeld et al 2007). The larger error in clinical studies than that in the phantom study is typically due to the in vivo conditions, e.g., patient tissue motion, tissue interfaces, which can displace the needle. In some cases pubic bones can also cause increased needle deflection. The result was also comparable to the needle-placement error in clinical studies on transrectal needle placement; Engelhard et al (2006) reported that the needle was successfully placed in suspected lesion less than 10 mm; Schouten et al (2012) compared their robotic device for transrectal biopsies and commercially available transrectal biopsy device in 13 clinical biopsy procedures resulting mean targeting error of 5.7 and 5.8 mm, respectively. However, our needle placement was not as accurate as the studies using thicker needles; Susil et al (2004) reported that the needle-placement accuracy was 2.1 mm in eight clinical transperineal high-dose-rate brachytherapy studies using a 14-gauge needle guided by 1.5 T MRI scanner; Woodrum et al (2010) demonstrated needle placement for transperineal laser ablation under a 3.0 T MRI scanner using a 14-gauge needle with the needle-placement error of 2.1 mm in their cadaveric study. This indicates that the deflection of the biopsy needle is a major concern in accurate needle placement.

The study also serves as an important engineering step toward clinical application of MRI-guided robotic transperineal prostate interventions, which is expected to improve ergonomics and accuracy in needle placement (Fischer et al 2008, Song et al 2012, Seifabadi et al 2012). We are currently developing an MRI-compatible needle-placement robot that works with the presented in-bore setup and the navigation software. The robot will be built into the clinical workflow, imaging, software operation and needle placement, which have been developed and proven clinically feasible in this study. Several groups have already demonstrated that remotely controlled MRI-compatible needle-placement robots improve the ergonomics of the operation. Muntener et al (2008) and Cunha et al (2010) developed a fully-automated needle-placement robot for seed delivery in brachytherapy, which does not require a radiologist to reach to the perineum in the closed in-bore space for manipulation of the needle. Recently, Yakar et al
(2011) and Schouten et al (2012), and Zangos et al (2011) demonstrated clinical application of remotely controlled MRI-compatible robots for positioning of needle guides in transrectal and transgluteal biopsies, respectively. These robots allow positioning and orienting the needle guides in the scanners remotely with real-time MRI guidance, making the targeting process ergonomically comfortable for operating physicians. The advantage of robotic operation over manual operation in terms of targeting accuracy has not been proven in the clinical trials yet (Schouten et al 2012). However, robots allows unique mechanical motion such as step-wise tapping of needles to reduce tissue dragging, potentially improving the needle-placement accuracy (van den Bosch et al 2010).

The limitation of this study is that we only considered geometrical error of needle placement by comparing the distance between the planned target and the actual needle position estimated from the confirmation image. A more complete analysis of clinical outcome should also take into account the inaccuracy due to misalignment secondary to prostate motion voluntary and involuntary between the preprocedural diagnostic image and intraprocedural image, and the deformation and displacement of the prostate gland during the biopsy procedure, which will be evaluated in future work.

In conclusion, we developed a prostate intervention table and software that support transperineal manual needle biopsies in a wide-bore 3T MRI scanner. The table is equipped with a template with a Z-shaped calibration frame that allows needle placement with an error of 5.4 mm in clinical biopsies. Our preclinical and early clinical studies have shown the technique to be feasible, given that the targeting error was comparable to the clinical studies in the literature. This approach allows for the site-specific pathological tissue analysis of focal MRI-detected abnormalities in the prostate gland.

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